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PART DESIGNATIONS ON CIRCUIT BOARDS

FT-101Z CIRCUIT BOARDS

The FT-101Z series integrates the "mother board" concept and the "plug-in" type of circuit card. Each circuit board used in the FT-101Z has a code number assigned to it, and each part within the transceiver has a part number assigned to it (e.g. Q₅₀₂).

Parts numbers 01–99 (e.g. R₁₂) are located on the main chassis. Other parts, located on the circuit boards, are assigned a three or four digit part number; the last two digits are the part number for that particular board, while the first one or two digits are the code number for the board.

Thus, Q₃₀₁ is transistor number 01, located on circuit board number 3, which is the PREMIX UNIT. Refer to the accompanying chart for a tabulation of the code numbers assigned to the various circuit boards used in the FT-101Z series.

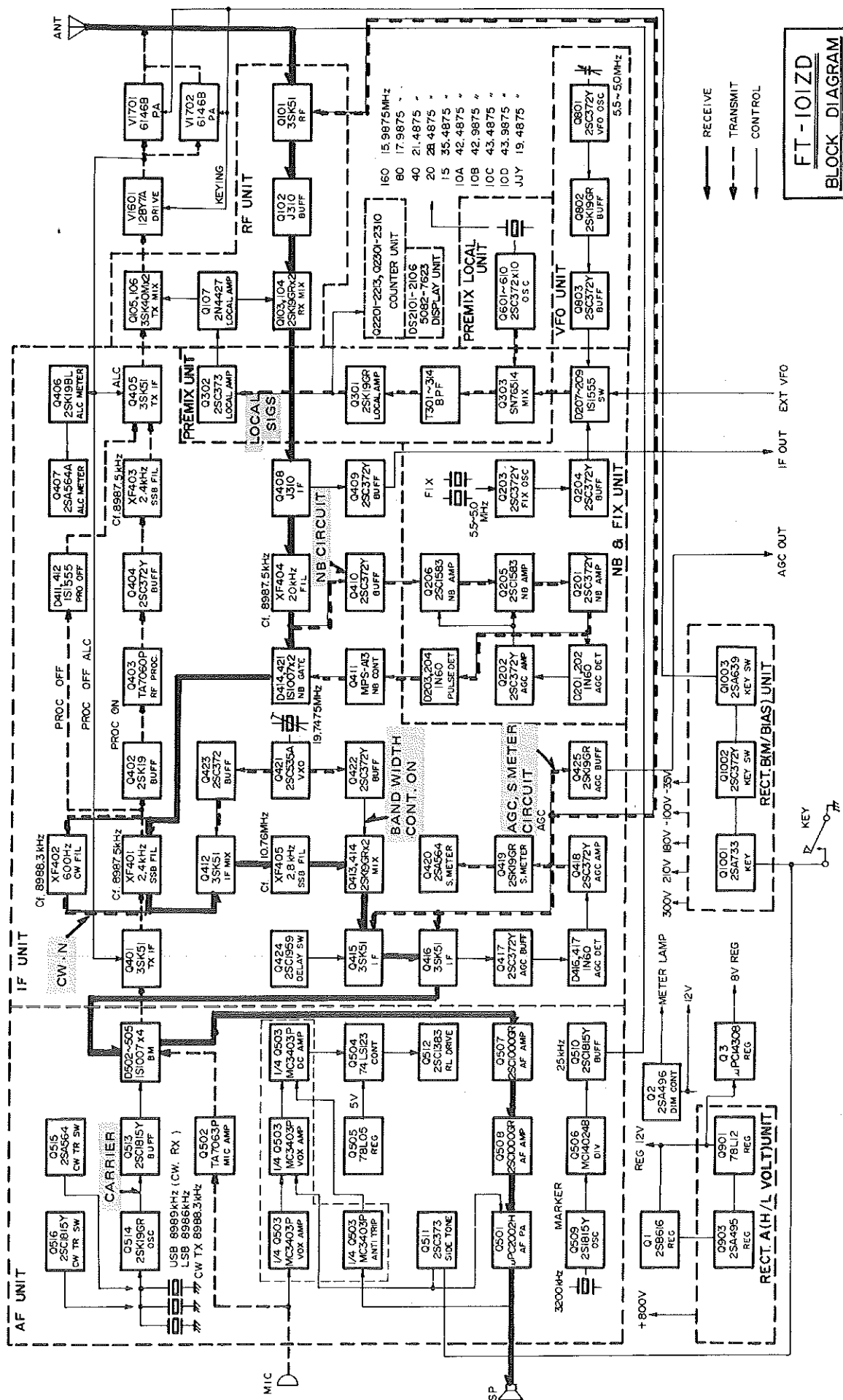
Code #	Unit	Board Designation
1	RF	PB-1960A
2	NB/FIX	PB-1961B
3	PREMIX	PB-1962A
4	IF	PB-1963B
5	AF	PB-1964A
6	PREMIX LOCAL	PB-1965
7	SELECT SW.	PB-1966C
8	VFO	PB-1440B-3420
9	RECT A	PB-1967
10	RECT B	PB-1968A
11	CAPACITOR	PB-1969A
12	TRIMMER A	PB-1970
13	TRIMMER B	PB-1970
14	TRIMMER C	PB-1092
15	BW CONT	PB-1972
16	DRIVER	PB-1714A
17	FINAL	PB-1715A
18	CLAR CONT	PB-1973A
19	LED	PB-1974A
20	LEVER SW	PB-1975A
21	DISPLAY	PB-1978
22	COUNT/DECODE	PB-1979
23	COUNTER MAIN	PB-1980
24	AM	PB-2040
32	DC-DC CONV	—

SIGNAL TRACING IN THE FT-101ZD

A highly useful signal in the FT-101ZD, one that can be used for most receiver alignment steps, is the internal calibrator. Fed into the receive line right at the antenna terminal, the calibrator signal should read about S9 + 10 dB, with the preselector peaked, at 14.200 MHz, SSB mode. While minor variations from this figure are no cause for alarm, a blown RF amplifier FET will cause this reading to be practically nil.

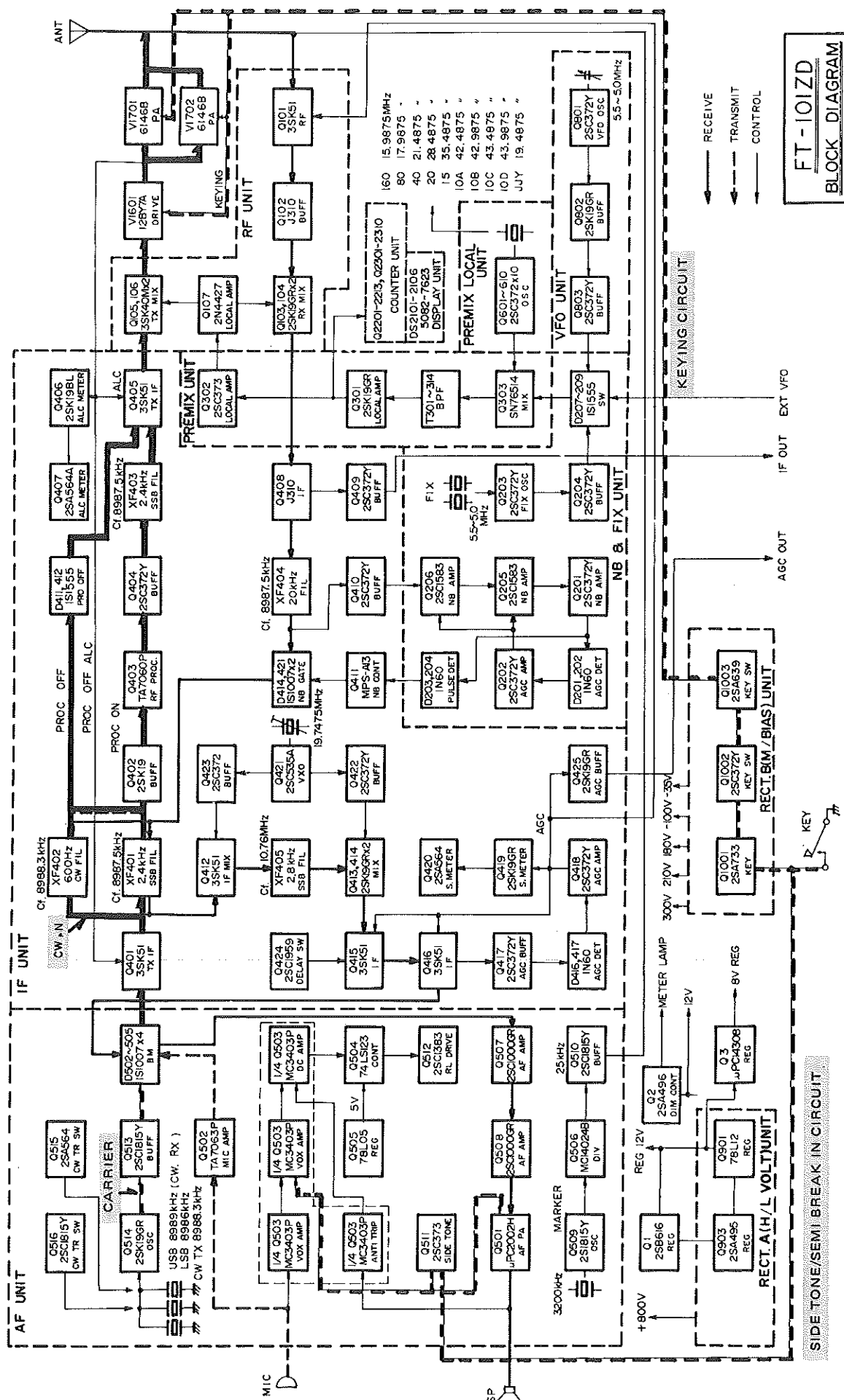
In the following section, we have presented augmented block diagrams which should help you in tracing the signal paths throughout the FT-101ZD. Armed with a couple of alignment wands and the calibrator signal, receiver peaking can be completed in short order, leaving you free to diagnose problems on the TX side.

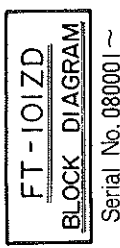
SSB/CW MODE RX



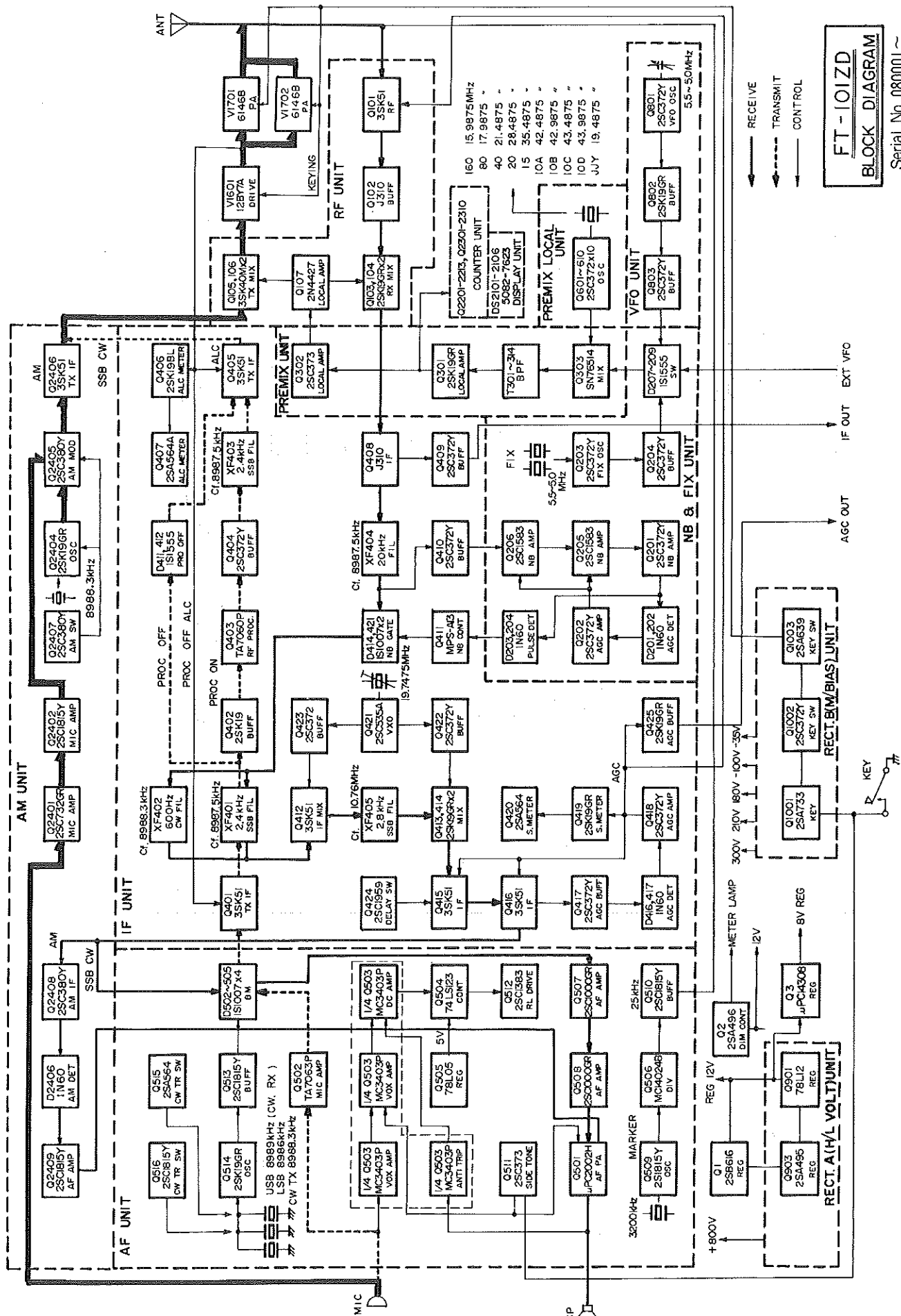


CW MODE TX



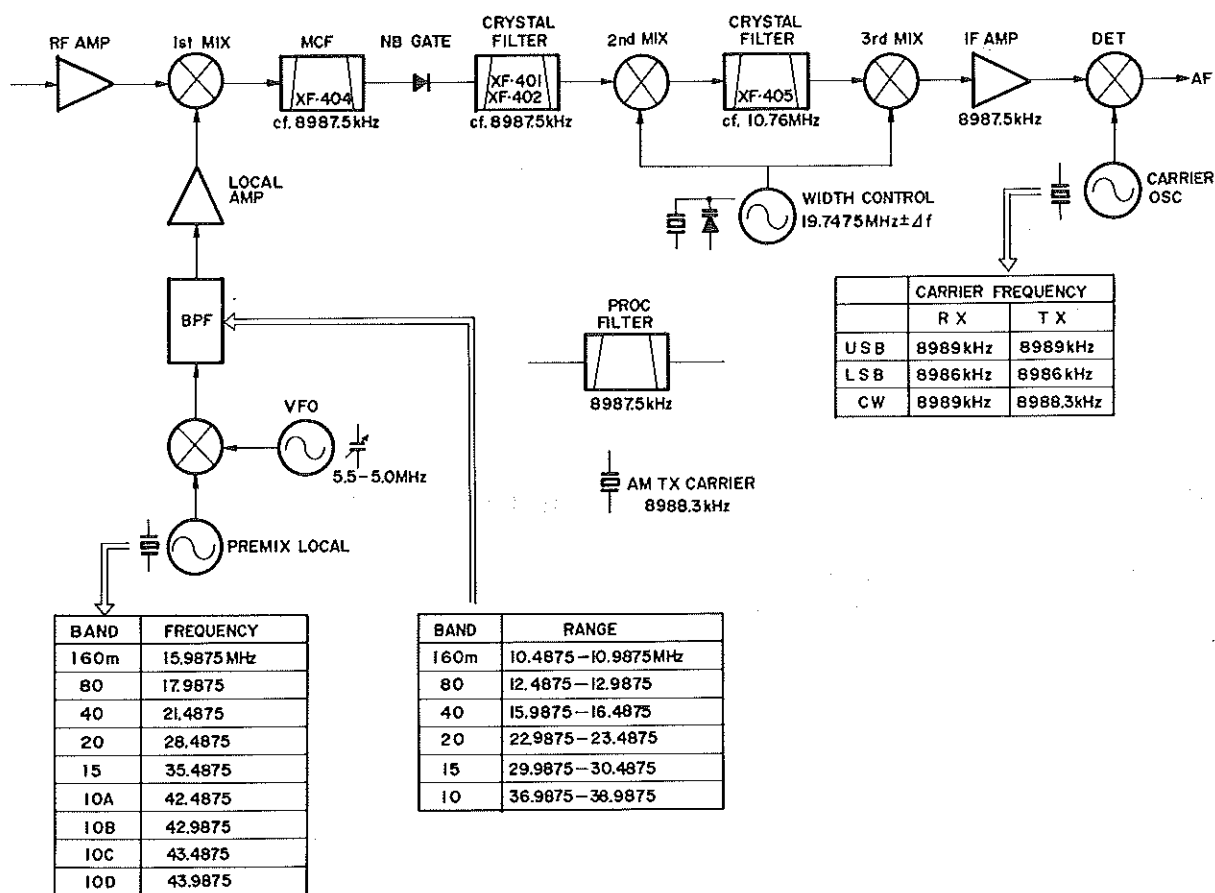


AM MODE TX



FT-101ZD
BLOCK DIAGRAM
Serial No. 080001~

FREQUENCY RELATIONSHIPS



CRYSTAL DATA FT-101ZD

UNIT	FUNCTION	HOLDER	FREQUENCY (kHz)	MODE	LOAD C (pF)	EFFECTIVE RESISTANCE	DRIVE LEVEL
CRYSTAL	160m	HC-18/U	15987.5	3rd overtone	30	80 (Ω)	2 mW
	80m	"	17987.5	"	"	60	"
	40m	"	21487.5	"	"	45	"
	20m	"	28487.5	"	"	40	"
	15m	"	35487.5	"	"	40	"
	10m (A)	"	42487.5	"	"	40	"
	10m (B)	"	42987.5	"	"	40	"
	10m (C)	"	43487.5	"	"	40	"
	10m (D)	"	43987.5	"	"	40	"
CARRIER	WWV(5MHz)	"	19487.5	"	"	40	"
	LSB	HC-18/U	8986	Fundamental	35	30	10mW
	USB	"	8989	"	"	35	"
	CW	"	8988.3	"	"	35	"
IF	AM	"	8988.3	"	"	35	"
	Width	"	★cf.19747.5	Fundamental	"	15	2 mW
COUNTER	Local	"	18000	"	"	15	10mW
	Local	"	18500	"	"	15	"
	Clock	HC-14/W	655.36	"	23	7K	2 mW
VOX/MARK	Marker	HC-6/W	3200	"	"	50	5 mW

★XCO FREQUENCY: 19743—19753kHz

Decided by circuit

CIRCUIT DESCRIPTION

The block diagram and following circuit description will provide you with a better understanding of the design of this transceiver. The circuit description is tailored to the full-feature FT-101ZD, and the reader should note that the counter unit and digital display are optional features for the FT-101Z.

The FT-101ZD consists of a premix-type single conversion system, using a 9 MHz IF for all modes of operation.

RECEIVER

The RF input signal from the antenna is fed through antenna relay RL₂, lamp fuse FH₂, attenuator switch S₂₀₀₄ (located on the LEVER SW unit, PB-1975), 9 MHz trap L₂₁₀₁ and C₁₂₀₇ (located on the TRIMMER A UNIT), and input transformer T₁ to pin 3 of the RF UNIT.

RF UNIT (PB-1960)

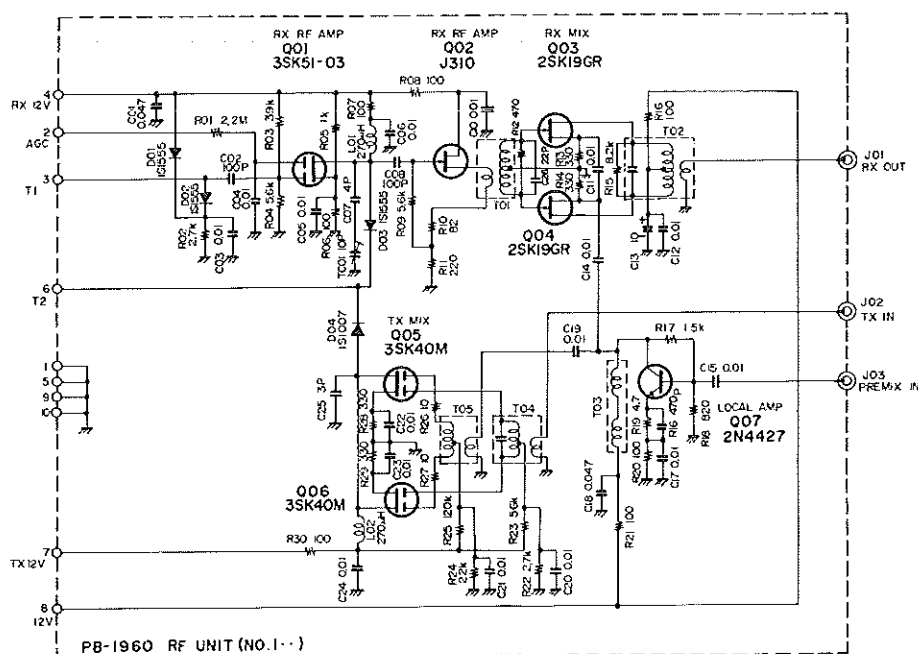
The incoming signal is amplified by the RF amplifier, Q₁₀₁ (3SK51-03), a dual-gate MOSFET used in a grounded source configuration. This transistor has superior immunity from intermodulation distortion. The amplified signal is then fed through a source follower, Q₁₀₂ (J310), to the

balanced mixer consisting of Q₁₀₃ and Q₁₀₄ (2SK19GR), where the input signal is heterodyned with the local oscillator signal. The local signal is delivered from buffer amplifier Q₁₀₇ (2N4427), and the resulting IF signal of 8.9875 MHz is fed through T₁₀₂ to J₁₀₁.

The input and output of the RF amplifier are permeability-tuned circuits, resulting in high sensitivity and excellent rejection of unwanted out-of-band signals.

IF UNIT (PB-1963)

The IF signal at pin 9 of J₄₀₃ is amplified by Q₄₀₈ (J310) and passed through a monolithic filter, XF₄₀₄, which has a ± 10 kHz bandwidth. The monolithic filter provides early protection from IMD, while providing a wide-bandwidth point for noise blanking. The IF signal is then fed to noise blanker gate D₄₀₄ (1S1007), which functions as an ON/OFF switch controlled by noise blanker driver Q₄₁₁ (MPSA13).



The IF signal is then passed through the SSB filter XF₄₀₁ (or optional CW filter XF₄₀₂). Selection of the filter to be used is made by diodes D₄₀₅ - D₄₀₈ (1S1007), depending on the mode of operation.

The IF signal is then fed to the IF first mixer, Q₄₁₂ (3SK51-03), where the incoming signal is heterodyned with a 19.7475 MHz $\pm \Delta f$ local signal delivered from crystal oscillator Q₄₂₁ (2SC535A) and buffer amplifier Q₄₂₃ (2SC372Y), resulting in a signal of 10.76 MHz $\pm \Delta f$.

The new 10.76 MHz $\pm \Delta f$ signal is fed through filter XF₄₀₅ to the IF second mixer, Q₄₁₃/Q₄₁₄ (2SK19GR), where the filtered signal is heterodyned with the 19.7475 MHz $\pm \Delta f$ signal delivered from Q₄₂₂ (2SC372Y), resulting in an 8.9875 MHz IF signal, the same as the original IF.

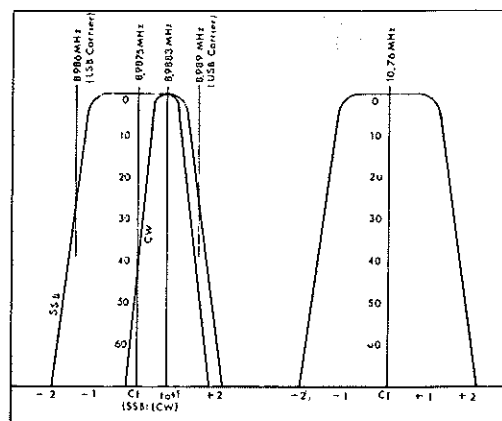
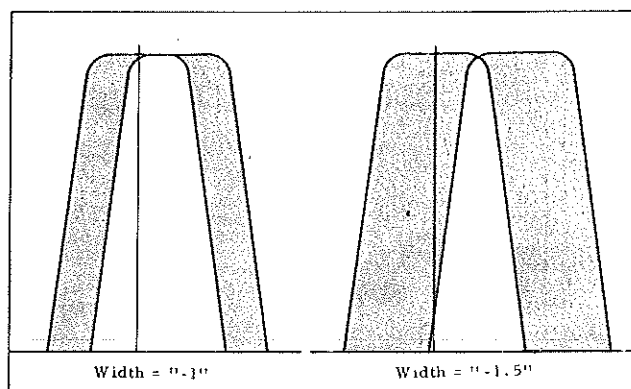
This process varies the IF signal across the passband of the second IF filter. The combination of the two filters, XF₄₀₁ and XF₄₀₅, provides continuously variable width of the IF passband. The frequency of crystal oscillator Q₄₂₁ is varied by varactor diode D₄₁₈ (1S2209).

The output from the IF second mixer is fed to a two-stage IF amplifier, consisting of Q₄₁₅ and Q₄₁₆ (3SK51-03), and delivered through diode switch D₄₀₁ (1S1555) to the AF UNIT.

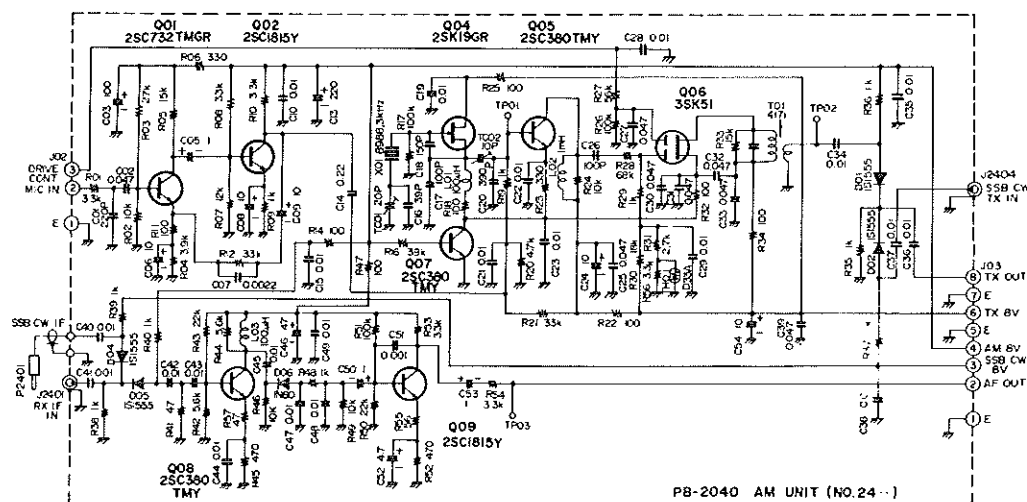
A portion of the output from Q₄₁₆ is rectified by D₄₁₆ and D₄₁₇ (1N60) to produce AGC voltage. Q₄₁₇ (2SC372Y) provides the necessary buffering between the IF and AGC circuits. The AGC voltage is amplified by Q₄₁₈ (2SC372Y), and applied to gate 2 of the RF and IF amplifiers, to control the gain of these stages. The AGC voltage is also amplified by Q₄₁₉ (2SK19GR) for S-meter indication.

For use with the FV-901DM scanning VFO, or other optional equipment, the AGC voltage is fed through buffer Q₄₂₅ (2SK19GR) and fed to the AGC OUT terminal on the EXT VFO jack, located on the rear panel.

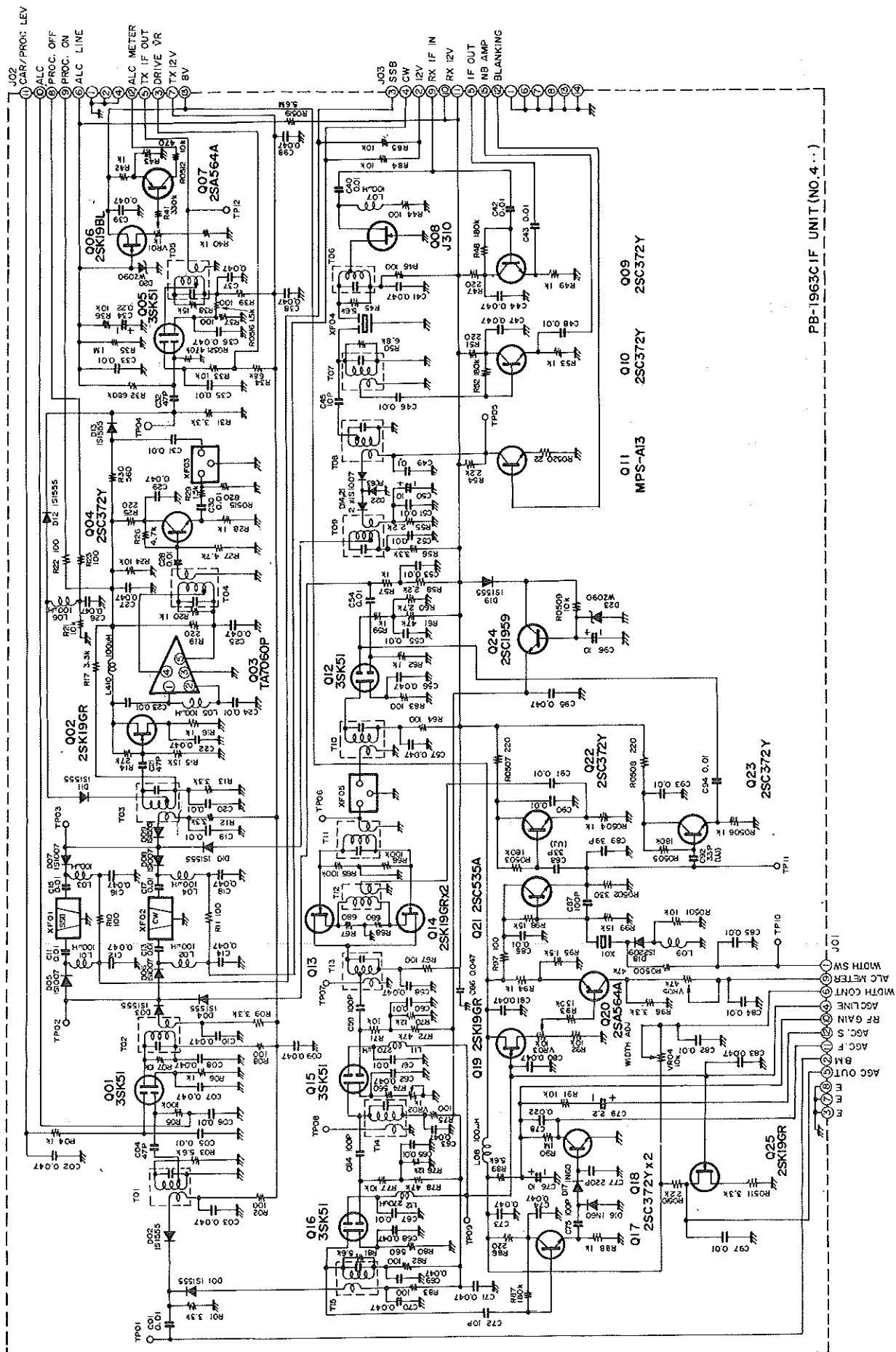
On AM, the output signal from Q₄₁₆ is amplified by Q₂₄₀₈ (2SC380Y) and passed to the AM detector, D₂₄₀₆ (1N60). The resulting audio signal is amplified by Q₂₄₀₉ (2SC1815Y) and delivered to the final audio stage.

SSB, CW
FiltersWIDTH
Filter

Width Control Action



TECHNICAL NOTES



NB-FIX UNIT (PB-1961)

A portion of the 8.9 MHz IF signal is fed through buffer Q_{410} (2SC372Y) and amplified by Q_{206} and Q_{205} (2SC1583).

When a carrier of noise-free modulated signal is received, the IF signal is rectified by D_{201} and D_{202} (1N60), producing a DC voltage. This DC voltage is amplified by Q_{202} (2SC372Y), which charges C_{214} , for AGC purposes. The AGC voltage is used to control the gain of Q_{206} and Q_{205} .

When impulse-type noise is received, D_{203} and D_{204} (1N60) rectify the IF signal, producing a DC voltage which controls the NB switch Q_{411} (2SC372Y).

Noise pulses have a very short duration, but high amplitude. Because of the very slow time constant of the C_{214}/R_{212} discharge path, AGC voltage is not induced by these short-duration pulses. Therefore, Q_{206} and Q_{205} operate at full gain, providing maximum voltage to the base of Q_{411} . When a pulse is received, Q_{411} biases D_{414} to block the signal path momentarily. When a desired signal and a noise pulse are received simultaneously, the blanking action is not impaired, because the relative amplitude difference between the desired signal and the noise pulse is still high. The front panel noise blanker level control varies the DC voltage applied to the base of Q_{411} .

AF UNIT (PB-1964)

The IF signal from pin 2 is fed through T_{501} to the ring demodulator, consisting of $D_{502} - D_{505}$ (1S1007), where the IF signal is demodulated into audio, using the carrier signal delivered from Q_{503} (2SC1815Y). The carrier signal is generated by oscillator Q_{514} (2SK19GR), and it oscillates at one of the following frequencies:

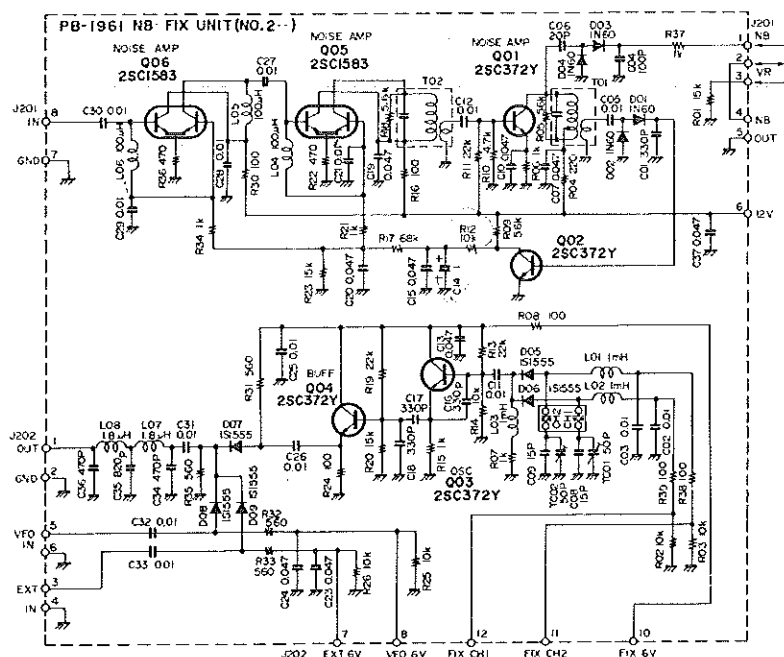
USB, CW-RX	8989 KHz
LSB	8986 KHz
CW-TX	8988.3 KHz

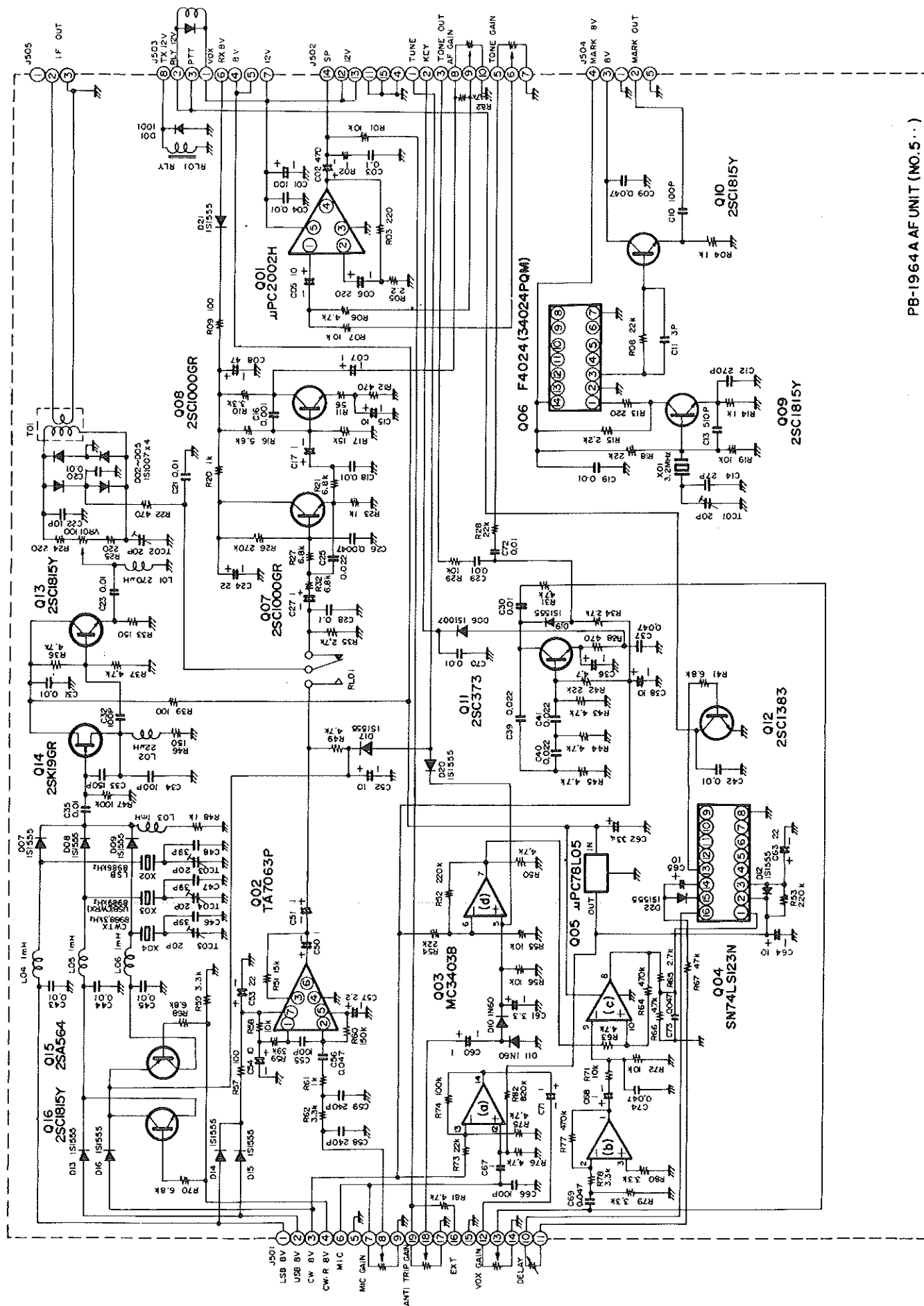
The audio signal is then amplified by audio amplifiers Q_{507} , Q_{508} (2SC1000GR), and Q_{509} (μ PC2002), delivering 3 watts of audio output to the speaker.

The audio spectrum is shaped by an active low-pass filter of $f_0 = 2.7$ kHz, -12 dB/octave.

MARKER GENERATOR

A 25 kHz marker signal is provided, for alignment and testing purposes. Marker generator Q_{509} (2SC1815Y) generates a basic 3200 kHz signal, which is divided into 25 kHz multiples by Q_{506} (MC14024B), a binary counter.





PB-1964A AF UNIT (NO.5...)

TRANSMIT CIRCUIT

SSB MODE

The output from microphone jack J_2 is fed through the MIC GAIN control VR_{3a} to pin 8 of the AF UNIT.

AF UNIT (PB-1964)

The speech signal from pin 8 is amplified by microphone amplifier Q_{502} (TA7063P) and fed through relay RL_{501} to the ring modulator, $D_{502} - D_{505}$, where the speech signal modulates the carrier signal delivered from Q_{513} . The resulting double sideband signal is fed to the IF UNIT.

IF UNIT (PB-1963)

The 8.9875 MHz double sideband signal is amplified by Q_{401} (3SK51-03) and passed through sideband filter XF_{401} by diode switches D_{403} , D_{409} (1S1555), D_{405} , and D_{407} (1S1007). Here the signal is converted to a single sideband signal by removal of the unwanted sideband.

The signal is then fed to buffer amplifier Q_{402} (2SK19GR). When the RF speech processor is OFF, diode switches D_{411} and D_{412} (1S1555) feed the IF signal to IF amplifier Q_{405} (3SK51-03). When the RF speech processor is ON, the SSB signal is amplified by buffer amplifier Q_{402} (2SK19GR) and further amplified by limiter Q_{403} (TA7060P), where signals that exceed the preset clipping level are sliced out.

This highly clipped SSB signal is amplified by buffer amplifier Q_{404} (2SC372Y) and passed through a selective filter, XF_{403} , which removes RF harmonics that result from signal clipping. The signal is then fed to IF amplifier Q_{405} , and subsequently delivered to the RF UNIT. The front panel COMP LEVEL control, VR_4 , controls the voltage at gate 2 of Q_{401} , thus setting the processor level.

The return of the grid circuit of the final amplifier tubes is fed to Q_{406} (2SK19BL), which produces ALC voltage. This voltage is fed to gate 1 of Q_{405} ,

controlling the gain of this stage. When the RF processor is off, ALC voltage is also fed to gate 1 of Q_{401} . Q_{407} (2SA564) amplifies the ALC voltage for indication on the front panel meter.

RF UNIT (PB-1960)

The IF signal is fed through T_{104} to the transmit mixer, consisting of parallel-connected Q_{105} and Q_{106} (3SK40M), where the IF signal at gate 1 is mixed with the local signal fed to gate 2, producing the RF output signal. The RF signal is then fed through diode switch D_{104} (1S1007) to the DRIVE UNIT.

DRIVE UNIT (PB-1714), PA UNIT (PB-1715)

The RF signal is amplified by driver V_{1601} (12BY7A), and delivered to PA UNIT final amplifier tubes V_{1701} and V_{1702} (6146B). The output from the final tubes is fed to the antenna jack.

A portion of the RF signal is coupled through C_{14} to the cathode of the 12BY7A driver, for the purpose of improving the linearity of the final amplifier. This technique is known as RF negative feedback.

CW MODE

For CW, the 8.9883 MHz carrier is generated by oscillator Q_{514} at the frequency set by X_{504} . The carrier signal is fed through buffer Q_{513} and fed to the ring modulator. The same carrier frequency is used in the tune mode.

DC voltage is applied through diode switch D_{517} (1S1555) and relay RL_{501} , unbalancing the ring modulator for CW operation. The carrier signal is then fed to the IF UNIT. The signal path is identical to that on SSB, up to the DRIVE UNIT.

DRIVE UNIT (PB-1714), PA UNIT (PB-1715)

Keying of the transmitter is accomplished by changing the bias voltage to the driver and final tubes. During "key up," the tubes are cut off by application of -35 volts to V_{1601} and -110 volts to V_{1701} and V_{1702} . These cutoff voltages are

TECHNICAL NOTES

reduced to -0.1 volt and -60 volts, respectively, during "key down" conditions.

The key is connected to the KEY 2 terminal on the RECT B board, PB-1968. When the key is closed, the base of Q_{1001} (2SA733) is grounded, causing Q_{1002} (2SC372Y) to conduct. The base of Q_{1003} (2SA639) is thus set to 0 when the transistor conducts. Under these circumstances, the bias voltage applied to V_{1601} , V_{1701} , and V_{1702} places these tubes in the normal operating condition.

VOX circuit

A portion of the microphone input signal is amplified by three stages of Q_{503} (MC3403P), which drive the VOX control gate, Q_{504} (SN74LS123N). The output from pin 13 of Q_{504} is fed to the base of Q_{512} (2SC1383), switching the VOX relay on and off according to the presence or absence of a speech signal.

A portion of the speaker output is detected by D_{510} and D_{511} (1N60), providing a bucking voltage which is fed to Q_{503} , preventing the speaker output from tripping the VOX.

The VOX delay may be set by adjusting VR_{2b} for the desired delay time.

CW SIDETONE

CW sidetone oscillator Q_{511} (2SC373) oscillates at a frequency of approximately 800 Hz. The output from Q_{511} is amplified by the final audio

amplifier, Q_{501} , for delivery to the speaker. The output from the sidetone oscillator is also fed to VOX amplifier Q_{503} , providing semi-break-in operation for CW.

AM MODE

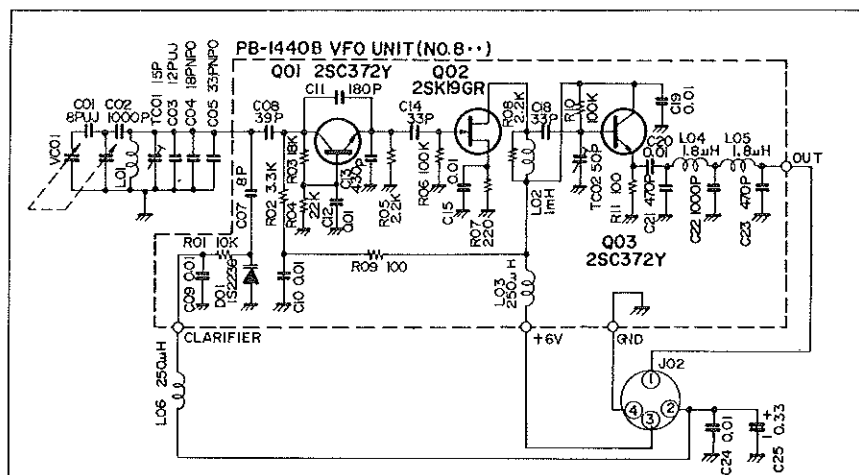
The speech signal from the microphone is amplified by Q_{2401} (2SC732GR) and Q_{2402} (2SC1815Y) and passed to modulator Q_{2405} (2SC380Y), where the speech signal modulates the AM carrier signal at 8988.3 kHz delivered from Q_{2404} (2SK19GR). The modulated signal is amplified by Q_{2406} (3SK51) and delivered to transmit mixer Q_{105}/Q_{106} .

COMMON CIRCUITS

VFO UNIT (PB-1440B-3420)

A modified Colpitts-type oscillator is used to generate a 5.0 - 5.5 MHz VFO signal, thus producing a 500 kHz tuning range. The oscillator signal generated by Q_{801} (2SC372Y) is varied by VC_{801} , which is geared to a precision-built dial tuning mechanism. VC_{801} consists of two sections; the sub-blades compensate for the capacitance variation of the main blades, which may result from extreme temperature change.

Varactor diode D_{801} (1S2209) may be varied by tuning L_{806} , providing ± 2.5 kHz offset from the dial frequency (clarifier).



The VFO signal is amplified by buffer amplifiers Q₈₀₂ (2SK19GR) and Q₈₀₃ (2SC372Y), and passed to the PREMIX UNIT.

NB & FIX UNIT (PB-1961)

Two crystal-controlled channels are provided for operation with this transceiver. The oscillator signal is generated by Q₂₀₃ (2SC372Y) and amplified by Q₂₀₄ (2SC372Y), and delivered to the PREMIX UNIT. Crystals X₂₀₁ and X₂₀₂ oscillate in the 5.0 - 5.5 MHz range.

PREMIX LOCAL UNIT (PB-1711)

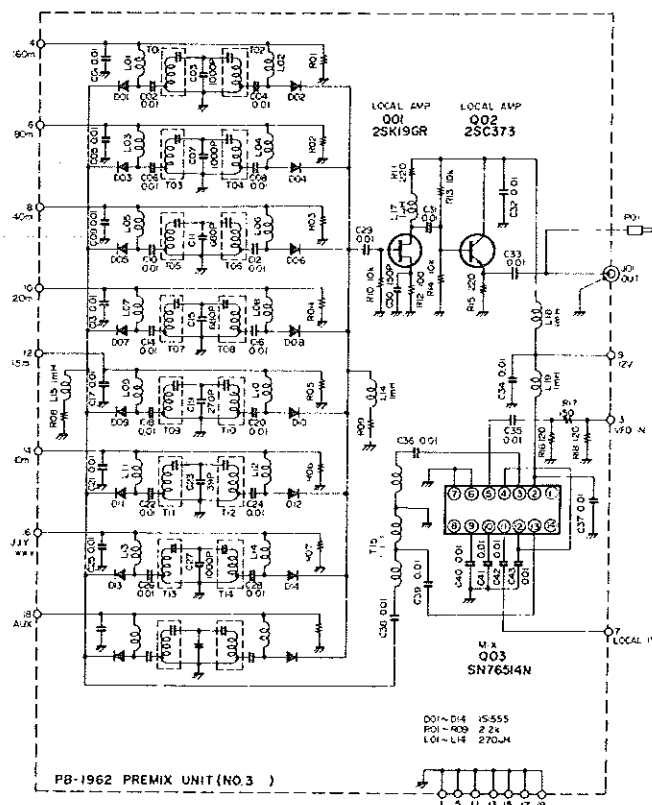
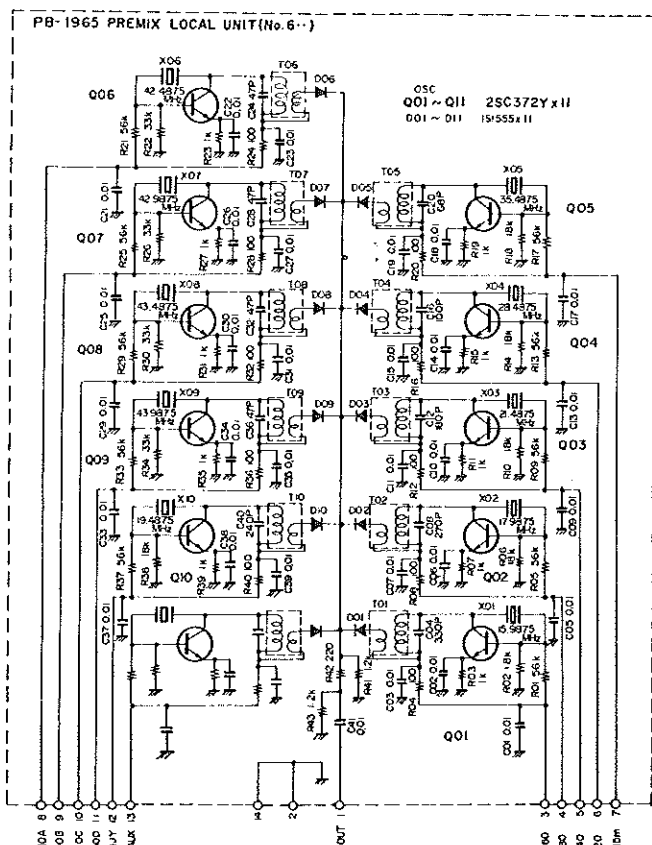
Crystal oscillators Q₆₀₁ - Q₆₁₀ (2SC372Y) generate the premix local signal at the frequencies shown in Table 3. Diode switches D₆₀₁ - D₆₁₀ (1S1555) select the proper local signal for the band in use. The local signal is then delivered to the PREMIX UNIT.

PREMIX UNIT (PB-1962)

The premix signal is produced at Q₃₀₃ (SN76514N), a double-balanced mixer, where the premix local signal from Q₆₀₁ - Q₆₁₀ is mixed with the VFO or crystal controlled 5 MHz signal. The premix output frequencies are shown in Table 3. The premix signal is passed through bandpass filter T₃₀₁ - T₃₀₄, and amplified by Q₃₀₁ (2SK19GR) and Q₃₀₂ (2SC373). The amplified signal is then fed to the RF UNIT, where the signal is further amplified by Q₁₀₇ for delivery to the transmitter and receiver mixers.

		XCO Frequency	PREMIX OUT Frequency
160m	X ₆₀₁	15.9875MHz	10.4875~10.9875MHz
80m	X ₆₀₂	17.9875MHz	12.4875~12.9875MHz
40m	X ₆₀₃	21.4875MHz	15.9875~16.4875MHz
20m	X ₆₀₄	28.4875MHz	22.9875~23.4875MHz
15m	X ₆₀₅	35.4875MHz	29.9875~30.4875MHz
10mA	X ₆₀₆	42.4875MHz	36.9875~37.4875MHz
10mB	X ₆₀₇	42.9875MHz	37.4875~37.9875MHz
10mC	X ₆₀₈	43.4875MHz	37.9875~38.4875MHz
10mD	X ₆₀₉	43.9875MHz	38.4875~38.9875MHz
JJY/ WWV	X ₆₁₀	19.4875MHz	13.9875~14.4875MHz

Table 3



COUNTER UNIT (PB-1978, PB-1979, PB-1980)

The premix local signal from the PREMIX LOCAL circuit is fed to amplifier Q_{2301} (3SK51-03), located on PB-1980. The amplified signal is then fed to waveshaper Q_{2302} (MC10116). Q_{2303} (MPS3640) acts as an interface between Q_{2302} and the TTL circuitry. The signal is then fed to the counter gate, Q_{2304} (SN74S00N).

The clock pulses are generated by Q_{2305} (MSM5564), which produces a 655.36 MHz signal. The signal is divided by a factor of 2^{17} , producing a 5 Hz signal which is fed to the counter gate.

The pulses which pass through the gate are fed to decade counter Q_{2309} (SN74196N), which counts 10 Hz digits. In turn, $Q_{2302} - Q_{2307}$ (SN74LS196N) count 100 Hz, 1 kHz, 10 kHz, 100 kHz, 1 MHz, and 10 MHz digits. The BCD output signal from $Q_{2302} - Q_{2307}$ is fed through drivers $Q_{2208} - Q_{1213}$ (MSM561) to the display digits, $DS_{2101} - DS_{2106}$ (HP 5082-7623).

The system of presetting the counter can best be explained by example. For a frequency of 3.500 MHz LSB, the premix local frequency is 12.486 MHz. The LSB preset code is 91.014.0. $12.486 + 91.0140.0 = 103.500$. The "1" digit on the left-hand side is dropped (overflow), and the "0" preceeding the "3" causes a blanking signal to be sent to the 10 MHz digit. The result is a frequency of 3.500 MHz, and this number is displayed.

For USB, the preset number is 91.011.0. For a frequency of 14.000 MHz USB, the manipulation is as follows: $91.011 + 22.989$ (Premix freq.) = 114.000. The first digit is the overflow digit, and the remaining digits are displayed. Note that the second digit from the left is not zero, so no blanking signal is sent to the 10 MHz digit.

For a CW or AM frequency of 21.000 MHz, the premix frequency is 29.9883, and the preset frequency is 91.011.7. The manipulation is: $91.011.7 + 29.9883 = 121.0000$. The first digit is dropped, and the remaining digits are displayed.

The preset frequencies are programmed by Q_{2307} and Q_{2308} (μ PA54H) and diode matrix $D_{2306} - D_{2312}$ (1S1555). Please refer to Table 5 for definition of the premix frequencies for the various bands.

The 5 volt supply is regulated by Q_{2310} (μ PC 14305) for the TTL circuitry. The DIM control controls the emitter/collector voltage at Q_{2201} (2SA496Y), to control the brightness of the digital display and lamps.

	10MHz	1MHz	100kHz	10kHz	1kHz	100Hz
	(Q_{2207})	(Q_{2206})	(Q_{2205})	(Q_{2204})	(Q_{2203})	(Q_{2202})
LSB	9	1	0	1	4	0
USB	9	1	0	1	1	0
CW AM	9	1	0	1	1	7

Preset Number

Table 4

	Nominal Premix Local Frequency	LSB	USB	CW / AM
160m	10.4875 - 10.9875 (MHz)	10.486 - 10.986 (MHz)	10.489 - 10.989 (MHz)	10.4883 - 10.9883 (MHz)
80m	12.4875 - 12.9875	12.486 - 12.986	12.489 - 12.989	12.4883 - 12.9883
40m	15.9875 - 16.4875	15.986 - 16.486	15.989 - 16.489	15.9883 - 16.4883
20m	22.9875 - 23.4875	22.986 - 23.486	22.989 - 23.489	22.9883 - 23.4883
15m	29.9875 - 30.4875	29.986 - 30.486	29.989 - 30.489	29.9883 - 30.4883
10mA	36.9875 - 37.4875	36.986 - 37.486	36.989 - 37.489	36.9883 - 37.4883
10mB	37.4875 - 37.9875	37.486 - 37.986	37.489 - 37.989	37.4883 - 37.9883
10mC	37.9875 - 38.4875	37.986 - 38.486	37.989 - 38.489	37.9883 - 38.4883
10mD	38.4875 - 38.9875	38.486 - 38.986	38.489 - 38.989	38.4883 - 38.9883

Table 5



POWER SUPPLY

The power supply is designed to operate from 100/110/117/200/220/234 volts AC. A DC-DC converter is an available option, providing operation from 13.5 volts DC. Insertion of the appropriate power plug into the rear panel receptacle makes the necessary connections for AC or DC operation.

When the transceiver is operated from a DC 13.5 volt power source, using the optional DC-DC converter, transistors Q₃₂₀₁ and Q₃₂₀₂ (T20A6) function as a low frequency oscillator, providing AC voltage at approximately 80 Hz to the power transformer. All of the tube heaters receive their power through the HEATER switch on the front panel. When the HEATER switch is OFF, voltage is still supplied to the receiver section, thus allowing continuous reception with reduced power consumption. The heaters of the two 6146B are connected in series to operate at 12 volts DC.

The 14 volt AC power delivered from the secondary winding of the power transformer is rectified by D₉₀₅ and D₉₀₆ (V06B). Voltage regulators Q₁ (2SB616), Q₉₀₁ (78L12), and Q₉₀₃ (2SA495) stabilize the DC supply at 12 volts. The supply voltage is further stabilized at 8 volts by Q₃ (μPC14308) for delivery to the counter, AF, and other units. The 6 volt supply for the VFO is provided through zener diode D₉₀₈ (WZ061), while the 5 volt supply for the TTL integrated circuits is provided by Q₅₀₅ (78L05).

The power amplifier plate voltage of +800 volts is supplied from the bridge-controlled doubler, located on the RECT. A UNIT, and consisting of D₉₀₁ - D₉₀₄ (10D10).

AC 190 volts is rectified by D₁₀₀₂ (10D10), producing 210 volts for the screen grid supply of the power amplifier tubes. The screen grid voltage for the driver tube is obtained by rectifying 250 volts AC at D₁₀₀₁ (10D10), producing 300 volts. This voltage is dropped to 180 volts by a resistor for delivery to the driver tube screen grid.

The 120 volt AC power from the transformer secondary winding is rectified by D₁₀₀₃ (10D10) in order to obtain -140 volts for the driver and final amplifier tube grid bias.

